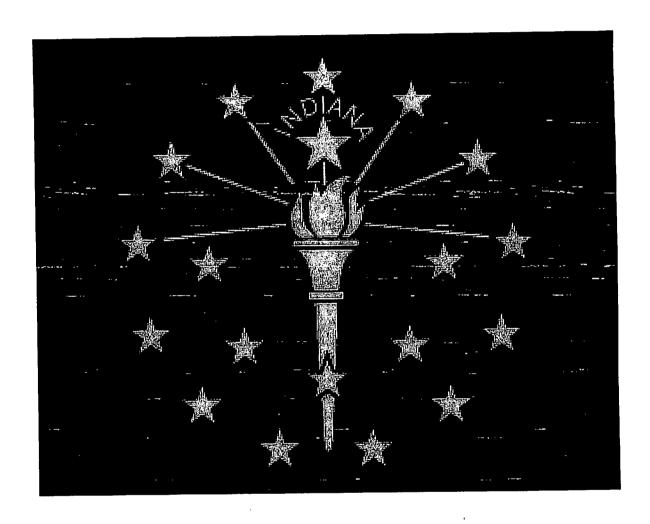
CLARK COUNTY



DRAINAGE ORDINANCE

SECTION 1 - PURPOSE AND INTENT

The purpose of this ordinance is to provide for the health, safety, and general welfare of the citizens of Clark County through the regulation of storm water runoff. This ordinance establishes guidelines for construction of residential and commercial properties within the jurisdiction of the Clark County Drainage Board.

SECTION 2 - ACRONYMS

For the purposes of this ordinance, the following shall mean:

Conservation Service)

1.	ASTM	American Society for Testing Materials
2.	CCDB	Clark County Drainage Board
3.	DGA	Dense Graded Aggregate
4.	FEMA	Federal Emergency Management Agency
5.	HAC	Hot Asphalt Concrete
6.	INDOT	Indiana Department of Transportation
7.	NGVD	National Geodetic Vertical Datum
8.	NRCS	USDA Natural Resources Conservation Service
9.	RCP	Reinforced Concrete Pipe
10.	SCS	Soil Conservation Service (now known as the USDA Natural Resources

SECTION 3 - DEFINITIONS

- 1. **ASTM**. American Society for Testing Materials, an association that publishes standards and requirements for materials used in the construction industry.
- 2. Blue Line Stream. Any stream depicted blue in color, solid or dashed, on a USGS Quad Map.
- 3. Capacity of a Storm Drainage Facility. The maximum flow that can be conveyed or stored by a storm drainage facility without causing damage to public or private property.
- 4. Catch Basin. A chamber usually built at the curb line of a street for the admission of surface water to a storm sewer or subdrain, having at its base a sediment sump designed to retain grit and detritus below the point of overflow.
- 5. Channel. A portion of a natural or artificial watercourse which periodically or continuously contains moving water, or which forms a connecting link between two bodies of water. It has a defined bed and banks, which serve to confine the water.
- 6. Contour. An imaginary line on the surface of the earth connecting points of the same elevation.
- 7. Contour Line. Line on a map, which represents a contour or points of equal elevation.
- 8. Crown of Pipe. The elevation of the top of pipe.
- 9. Culvert. A closed conduit used for the conveyance of surface drainage water under a roadway, railroad, canal or other impediment.
- 10. Datum. Any level surface to which elevations is referred, usually using Mean Sea Level.
- 11. Dense Graded Aggregate. Indiana No. 9 Crushed Stone.
- 12. **Design Storm**. A selected storm event, described in terms of the probability of occurring once within a given number of years, for which drainage of flood control improvements are designed and built.
- 13. **Detention**. Managing storm water runoff by temporary holding and controlled release.

- Detention Basin. A facility constructed or modified to restrict the flow of storm water to a prescribed maximum rate, and to detain concurrently the excess waters that 14. accumulated behind the outlet.
- Detention Storage. The temporary detaining of storm water in storage facilities, on rooftops, in streets, parking lots, school yards, parks, open spaces or other areas under 15. predetermined and controlled conditions, with the rate of release regulated by appropriately installed devices. (Refer to Section 8).
- Detention Time. The theoretical time required to displace the contents of a tank or unit at a given rate of discharge (volume divided by rate of discharge). 16.
- Discharge. Usually the rate of water flow. A volume of fluid passing a point per unit time commonly expressed as cubic feet per second, cubic meters per second, gallons per 17. minute, or millions of gallons per day.
- Drainage Area. The area draining into a stream at a given point. It may be of different sizes for surface runoff, subsurface flow and base flow, but generally the surface runoff 18. area is considered as the drainage area.
- Drainage Board. The Clark County Drainage Board 19.
- Drainage Improvement. An activity within or adjacent to a natural stream or a man-made drain primarily intended to improve the flow capacity, drainage, erosion and 20. sedimentation control, or stability of the drainage way.
- Drop Inlet. A structure in which water drops through a vertical riser connected to a 20. discharge conduit or storm sewer.
- Earth Embankment. A man-made placement of soil, rock, or other material often used 21. to form an impoundment.
- Easement. A right of use over designated portions of the property of another for a 22. clearly specified purpose.
- Emergency Spillway. Usually a vegetated earth channel used to safely convey flood 23. discharges around an impoundment structure.
- Flood Elevation. The maximum level of high waters for a flood of a given return period 24. and rainfall duration.
- Flood or Flood Water. Water that overflows the banks of a lake or watercourse. 25.
- Flood Hazard Area. Any floodplain, floodway, floodway fringe, or any combination which is subject to inundation by the regulatory flood elevation or any floodplain as 26. delineated by Zone A on the current Flood Hazard Boundary Map of the Federal Emergency Management Agency.
- Floodplain. The area adjoining the river or stream that has been or may be covered by floodwaters. It consists of both the floodway and the floodway fringe. 27.
- Floodway. The channel of a river or stream and those portions of the flood plains adjoining the channel, which is reasonably required to, efficiently carry and discharge the 28. peak flow of the regulatory flood of any river or stream.
- Floodway Fringe. That portion of the floodplain lying outside the floodplain lying, 29. which is inundated by the regulatory flood.
- Grade. (1) The slope of a road, a channel, or natural ground. (2) The finished surface of a canal bed, roadbed, top of embankment, or bottom of excavation; any surface prepared 30. to a design elevation for the support of construction, such as paving or the laying of a conduit. (3) To finish the surface of a channel bed, roadbed, top of embankment, or bottom of excavation, or other land area to a smooth, even condition.
- Head. (1) The height of water above any plane of reference. (2) The energy, either kinetic or potential, possessed by each unit weight of a liquid, expressed as the vertical 31.

- height through which a unit would have to fall to release the average energy possessed. Used in various compound terms, such as pressure head or velocity head.
- 32. Head Loss. Energy loss due to friction, eddies, changes in velocity, elevation, or direction of flow.
- 33. Headwater. (1) The source of a stream. (2) The water upstream from a structure or point on a stream.
- 34. Hydrograph. A graph showing for a given point on a stream the discharge, stage (depth), velocity, or other property of water with respect to time.
- 35. INDOT. Indiana Department of Transportation. Generally used here to refer to specifications contained in the publication "INDOT Standard Specifications."
- 36. NGVD. A particular elevation datum known as the National Geodetic Vertical Datum of 1929 (NGVD 1929).
- 37. Inlet. An opening into a storm sewer system for the entrance of surface storm water runoff more completely described as a storm sewer inlet.
- 38. Invert. The inside bottom of a culvert or other conduit.
- 39. Manhole. Storm sewer structure through which a person may enter to gain access to a storm sewer or enclosed structure. A manhole may also be an inlet for the storm sewer system.
- 40. Professional Land Surveyor. A person licensed under the laws of the State of Indiana to practice land surveying.
- 41. Professional Engineer. A person licensed under the laws of the State of Indiana to practice professional engineering.
- 42. Rainfall Intensity. The rate at which rain is falling at any given instant, usually expressed in inches per hour.
- 43. Rational Method. A means of computing storm drainage flow rates (Q) by use of the formula Q = CIA, where C is a coefficient describing the physical drainage area, I is the rainfall intensity and A is the area.
- 44. Regulatory Flood. A flood with a peak having a probability of occurrence of one (1) percent in any given year, which is commonly referred to as a one hundred (100) year flood as calculated by a method and procedure, which is acceptable to the Board. If a permit for construction in a floodway is required by the Indiana Department of Natural Resources, the regulatory peak discharge must be calculated by the method and procedure acceptable to the Board and the Indiana Department of Natural Resources.
- 45. Regulatory Floodway. The channel of a river or stream and those portions of the floodplain adjoining the channel which are reasonably required to carry and discharge the peak flow of the regulatory flood of any river or stream.
- 46. Retention Facility. A facility designed to completely retain a specified amount of storm water runoff without release except by means of evaporation, infiltration or pumping.
- 47. Runoff. That portion of precipitation that flows from a drainage area on the land surface, in open channels, or in storm water conveyance systems.
- 48. Sinkholes. A sinkhole is any closed depression in a limestone region formed by the removal of water, surficial soil, rock or other material that is connected to a cavern or underground passage. The sinkhole drainage area shall include any area that contributes surface water directly to the sinkhole.
- 49. Slope. Degree of deviation of a surface from the horizontal, measured as a numerical ratio or percent. Expressed as a ratio, the first number is commonly the horizontal distance (run) and the second is the vertical distance (rise) e.g., 2:1. However, the preferred method for designation of slopes is to clearly identify the horizontal (H) and

vertical (V) components (length (L) and Width (W) components for horizontal angles). Also note that according to international standards (Metric), the slopes are presented as the vertical or width component shown on the numerator - e.g., 1V: 2H. Slope expressions in this handbook follow the common presentation of slopes - e.g., 2:1 with the metric presentation shown in parenthesis - e.g., (1V: 2H). Slopes can also be expressed in Apercents≅. Slopes given in percents are always expressed as (100V/H) -e.g.; a 2:1 (1V: 2H) slope is a 50% slope.

50. Soil. The unconsolidated mineral and organic material on the immediate surface of the earth that serves as a natural medium for the growth of land plants. Also see alluvial soil, Clay, Cohesive soil, Loam, Permeability (soil), Sand, Silt, Soil horizon, Soil profile,

Subsoil, Surface soil, Topsoil.

51. Storm Event. An estimate of the expected amount of precipitation within a given period of time. For example, a 10-yr. frequency, 24-hr. duration storm event is a storm that has a 10% probability of occurring in any one year. Precipitation is measured over a 24-hr. period.

52. Storm Frequency. The time interval between major storms of predetermined intensity

and volumes of runoff - e.g., a 5-yr., 10-yr. or 20-yr. storm.

53. Storm Sewer. A sewer that carries storm water, surface drainage, street wash, and other wash waters but excludes sewage and industrial wastes. Also called a storm drain.

- 54. Storm water. Any surface flow, runoff, and drainage consisting entirely of water from any form of natural precipitation, and resulting from such precipitation.
- 55. Surface Runoff. Precipitation that flows onto the surfaces of roofs, streets, the ground, etc., and is not absorbed or retained by that surface but collects and runs off.
- 56. Time of Concentration (Tc). The travel time of a particle of water from the most hydraulically remote point in the contributing area to the point under study. This can be considered the sum of an overland flow time and times of travel in street gutters, storm sewers, drainage channels, and all other drainage ways.
- 57. Watershed Area. All land and water within the confines of a drainage divide.
- 58. Zoning Ordinance. Clark County Indiana Zoning Ordinance or any replacement zoning ordinance and its amendments.

SECTION 4 - GENERAL PROVISIONS

APPLICABILITY

- 1. All new development and redevelopment activities that result in the disturbance of one (1) or more acres of land within the jurisdiction of Clark County, Indiana, including land disturbing activities on individual lots on less than one (1) acre as part of a larger common plan of development of sale shall develop detailed construction plans, which includes provisions necessary for minimizing the impact of runoff from the proposed land use. The following exceptions area as follows:
 - 1. Projects that require only individual Improvement Location Permits for a single family dwelling, a two-family dwelling, or their accessory structures are not subject to these requirements.
 - 2. Projects that are agricultural structures in locations included in current soil and waster conservation plans that have been approved by the Clark County Soil and Water Conservation District are also exempt from these requirements.

The provisions of this section shall be deemed as additional requirements to the minimum standards required by other ordinances of the county. In the case of

conflicting requirements, the most restrictive shall apply.

Variations and Exceptions to this Ordinance: 3.

- 1. Whenever strict compliance with these regulations would result in extraordinary hardship or injustice to the developer because of unusual topography, unusual size or shape of the property, or unusual conditions in surrounding property or development, the CCDB may modify, vary or waive such regulation in order that the developer may subdivide or develop his property in a reasonable manner provided that such modification, variation or waiver will not nullify the intent or purposed of this ordinance and that the public welfare, interest of the CCBD and the surrounding area shall be protected. Any such variance, together with reasons therefore shall be entered up the minutes of the CCDB.
- 2. In granting modification, variations or wavers, the CCDB may impose such other reasonable conditions as well, in its judgment, in order to justify such modification, variation or waiver and still maintain the objectives of these regulations.
- 3. It shall be the developer's burden (or an agent thereof) to explain in writing the reasons or justifications for any such request to make any modifications, variations or waivers to these regulations.

RESPONSIBILITY FOR ADMINISTRATION

The Clark County Drainage Board (CCDB) shall administer, implement, and enforce the provisions of this ordinance. Any powers granted or duties imposed upon the CCDB may be delegated in writing by the Drainage Board to the enforcement personnel.

SEVERABILITY

The provisions of this ordinance are hereby declared to be severable. If any provision, clause, sentence, or paragraph of this Ordinance or the application thereof to any person, establishment, or circumstances shall be held invalid, such invalidity shall not affect the other provisions or application of this Ordinance.

ULTIMATE RESPONSIBILITY

The standards set forth herein and promulgated pursuant to this ordinance are minimum standards.

NOTICE OF VIOLATION

Whenever the Clark County Drainage Board finds that a person or entity developer has violated or failed to meet a requirement of this Ordinance, a written notice of such violation(s) shall be issued with 20 days to the responsible person or entity.

APPEAL OF NOTICE OF VIOLATION

Any person receiving a Notice of Violation may appeal the determination of the CCDB. The notice of appeal must be received within 10 calendar days from the date of the Notice of Violation. Hearing on the appeal before the CCDB shall take place within 30 calendar days from the date of receipt of the notice of appeal.

ENFORCEMENT MEASURES AFTER APPEAL

If the violation has not been corrected pursuant to the requirements set forth in the Notice of Violation, or, in the event of an appeal, within five days of the decision of the CCDB, the CCDB

The rainfall intensity factor, I, should be obtained from the Louisville, Kentucky Rainfall Intensity-Duration Curves.

The time of concentration (Tc) to be used shall be the sum of the inlet time and flow time in the drainage facility from the most remote part of the drainage area to the point under consideration. The flow time in the storm sewers may be estimated by the distance in feet divided by velocity of flow in feet per second. The velocity shall be determined by the Manning's Formula. Inlet time is the combined time required for the runoff to reach the inlet of the storm sewer. It includes overland flow time and flow time through established surface drainage channels such as swales, ditches and sheet flow across such areas as lawns, fields and other graded surfaces.

The time of concentration, Tc, shall be determined by calculating the time for a particle of water to travel from the most hydrological remote point of the project area to the point of interest.

Time of concentration to the first inlet or structure may be estimated by the Kirpick Equation (Tc = 0.0078*L^0.77*s^-0.385) where L equals length of travel in feet and S equals slope in foot per foot. Other methods to derive time of concentration such as TR-55, Kerby's Equation and the Kinematic Wave method will be acceptable. The minimum Tc shall not be less than 10 minutes. Manning's Equation should be used to estimate any in-pipe or channel travel.

Guidance to selection of the runoff coefficient "C" is provided by Table 1, which shows values for different types of surface and local soil characteristics. The composite "C" value used for a given drainage area with various surface types shall be the weighted average value for the total area calculated from a breakdown of individual areas having different surface types.

A listing of soils groups with their corresponding Hydraulic Soil Group can be found in the Appendix. They are classified into four categories: A, B, C, and D.

DESIGN FLOWS

The Professional Engineer or Professional Land Surveyor shall refer to the Ten State Standards for design methodology for storm sewers. The exception being that all storm sewer systems will be designed for the 10-year event. At a minimum, the facility must have the capacity to transport the 10-year post-development discharge except in unusual cases, such as retrofit projects. The CCDB shall determine design criteria for retrofit projects or other unusual cases. The water surface profile and through system capacity shall be checked for the 100-year post-development discharge. All drainage systems shall be capable of passing the 100-year design flow within the drainage easement. Additional facility specific requirements are found in the following portions of this ordinance.

TABLE 1 RUNOFF COEFFICIENTS BASED ON LAND USE, SOIL GROUPS AND SLOPE RANGE (%)

HYDRAULIC S	SOILS GROU	JP
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			Α			В			С			D	
		S	LOPE	%	S	LOPE	%	SI	OPE	%	SL	OPE %	6
LAND USE	% IMP	0-2	2-7	7+	0-2	2-7	7+	0-2	2-7	7+	0-2	2-7	7+
Residential	25	.31	.35	.39	.33	.38	.43	.37	.41	.48	.40	.44	.52
	38	.42	.45	.49	.44	.48	.52	.47	.50	.56	.50	.53	.59
	65	.65	.67	.69	.66	.68	.71	.68	.70	.73	.69	.71	.75
	75	.73	.75	.77	.75	.76	.78	.76	.77	.79	.77	.78	.80
Commercial Business	85	.82	.83	.84	.83	.84	.85	.84	.85	.86	.84	.85	.86
Industrial	72	.71	.73	.74	.72	.74	.76	.73	.75	.77	.75	.76	.79
Roofs, Driveways, Streets, etc.	100	.95	.95	.95	.95	.95	.95	.95	.95	.95	.95	.95	.95
Open Spaces, Lawns, Parks	' 0	.09	.15	.21	.13	.19	.26	.18	.23	.32	.22	.27	.37
Woodlands	0	.09	.15	.20	.13	.18	.23	.17	.22	.26	.20	.25	.30
Pasture, Grass and Farmland 0		.15	.20	.25	.18	.23	.30	.22	.26	.35	.25	.30	.40
Newly Graded/Disturbed		.65	.67	.69	.60	68.	.71	.68	3 .70	.73	.69	.71	1 .75

Soil Groups

Soil properties influence the relationship between rainfall and runoff by affecting the rate of infiltration. NRCS divides soils into four hydrologic soil groups based on infiltration rates (Groups A-D). Remember to consider effects of urbanization on soil groups as well.

Group A – Group A soils have a low runoff potential due to high infiltration rates even when saturated (0.30 in/hr to 0.45 in/hr or 7.6 mm/hr to 11.4 mm/hr). These soils primarily consist of deep sands, deep loess, and aggregated silts.

Group B - Group B soils have a moderately low runoff potential due to moderate infiltration rates when saturated (0.15 in/hr to 0.30 in/hr or 3.8 mm/hr to 7.6 mm/hr). These soils primarily consist of moderately deep to deep, moderately well to well drained soils with moderately fine to moderately coarse textures (shallow loess, sandy loam).

Group C – Group C soils have a moderately high runoff potential due to slow infiltration rates (0.05 in/hr to 0.5 in/hr or 1.3 mm/hr to 3.8 mm/hr if saturated). These soils primarily consist of soils in which a layer near the surface impedes the downward movement of water or soils with moderately fine to fine texture such as clay loams, shallow sandy loams, soils low in organic content, and soils usually high in clay.

Group D - Group D soils have a high runoff potential due to very slow infiltration rates (less than 0.05 in./hr or 1.3 mm/hr if saturated). These soils primarily consist of clays with high swelling

potential, soils with permanently high water tables, soils with a claypan or clay layer at or near the surface, shallow soils over nearly impervious parent material such as soils that swell significantly when wet or heavy plastic clays or certain saline soils.

Effects of Urbanization – The design professional should consider the effects of urbanization on the natural hydrologic soil group. If heavy equipment can be expected to compact the soil during construction or if grading will mix the surface and subsurface soils, the designer should make appropriate changes in the soil group selected. Soil types with their corresponding hydrologic soil groups can be found in the Appendix – Section 3.

SECTION 6 - STORM SEWER DESIGN STANDARDS

The 100-year discharge elevation must be checked for all locations to avoid flood damage to adjacent structures. Manning's Equation is recommended to calculate pipe flow and velocity. The storm sewer hydraulic grade line for the 100-year event shall be contained within the storm sewer system.

Hydraulic Capacity

The hydraulic capacity of storm sewers shall be determined using Manning's Equation:

 $Q = 1.486 R^{2/3} S^{1/2} A$

n

Q = volumetric flowrate (cfs)

R = the hydraulic radius in feet

S = the slope of the energy grade line in feet per foot

n = roughness coefficient (for reinforced concrete pipe, n = 0.012)

A = cross-sectional area (Ft²)

Roughness coefficient (n) values for other sewer materials can be found in standard hydraulics texts and references.

Minimum Size:

To minimize the potential for pipes to become clogged, the minimum size of all storm sewers shall be 12 inches. This does not pertain to outlet structures for detention/retention basins. (The rate of release for detention storage shall be controlled by an orifice plate of other devices, subject to approval of the Board, where the 12-inch pipe will not limit rate of release as required.)

Grade:

Sewer grade shall be such that, in general, a minimum of 18 inches of cover will be maintained over the top of the pipe when reinforced concrete pipe is used. Pipes with less cover than the minimum may be used only upon approval of the Board. Uniform slopes shall be maintained between inlets, manholes and inlets to manholes. Final grade shall be set with full consideration of the capacity required, sedimentation problems and other design parameters. Minimum and maximum allowable slopes shall be those capable of producing velocities of two and 15 feet per second, respectively, when the sewer is flowing full.

National Transportation Product Evaluation Program (NTPEP) and can be found at www.ntpep.org. Joints shall be an integral bell and spigot with rubberize gasket conforming to ASTM F477 unless otherwise noted. Alternatively, plain-end pipe connected with accompanying split-coupler can be used for driveway and culverts.

Pipe Bedding, Backfill and Surface Restoration:

All concrete pipes must be bedded according to the detail in the Appendix – Section 4, but not limited to the following:

- 1. Where pipe is installed in earth areas, not immediately adjacent to a street or road, place Indiana No. 9 crushed stone to the spring line for RCP. The remainder of the trench must be backfilled with selected earth materials, humped over the trench to allow for settling.
- 2. Where pipe is installed in a graveled area, the remainder of the trench must be backfilled with Indiana No. 9 to a point eight (8) inches below original grade.
- 3. Where pipe is installed in an asphalt street, driveway, or parking area, the remainder of the trench must be backfilled with Indiana No. 9 to the subgrade. The trench must then be trimmed back six (6) inches on each side and filled with 3000-psi concrete. After all construction is completed, the trench must be cleaned, primed and paved with a one (1) inch compacted thickness of INDOT HAC Surface to be flush with the surrounding area. All patch seams can only be saw cut, cut smooth, straight and tarred.
- 4. Where pipe is installed in a concreted area, the remainder of the trench must be backfilled with DGA to a point nine (9) inches below original grade. The trench must then be trimmed back six (6) inches along each side and filled with 3000-psi concrete flush with original grade. All patch seams must be saw cut only, smooth and straight.
- 5. All cutting of trenches in existing asphalt or concrete pavements must be done with a saw only to provide a straight, smooth joint when new paving is done.
- 6. In areas where rock is encountered, all rock shall be removed from the trench. Voids created by such removal shall be refilled with Indiana No. 9 crushed stone.
- 7. Before placing of the aggregate base course, the upper six inches of all subgrade and subbase shall be compacted to a minimum of ninety five (95) percent of maximum dry density as determined in accordance with AASHTO T99, as modified in 203.24.

All HDPE pipe shall be installed and bedded according to the manufacture's specifications. Installation of each product shall conform to approved Clark County installation specifications and details. When necessary, additional guidelines shall conform to either:

- INDOT specifications and standard drawings,
- ASTM D2321, standard installation for thermoplastic pipe, or
- Published manufacturer's installation guidelines.

For all pipe bedding details, refer to the detail in the Appendix - Section 4 of this ordinance.

SECTION 7 - OPEN CHANNEL DESIGN STANDARDS

This section describes the technical criteria necessary to design storm water channels and ditches using conventional design procedures. These procedures shall be applied to roadside and rear yard ditches and highly urbanized channel. All blue line streams (especially in undisturbed areas) shall be designed using Natural Channel Design techniques, if possible. This criterion represents minimum

requirements.

Manning's equation is required, except in cases where backwater conditions are significant. All calculations must be submitted for review.

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Channels and ditches should be capable of conveying the 10-year storm flow within their banks. Through drainage systems (culverts, storm sewers, etc.) shall generally be designed to collect and transport the post-development rate of runoff for the 10-year design storm. In all cases, the 100-year discharge elevation shall be checked to ensure that adjacent structures do not suffer flood damage.

All through systems constructed must be capable of passing the 100-year design flow within the drainage easement.

All open channels, whether private or public, and whether constructed on private or public land, shall conform to the design standards and other design requirements contained herein.

Manning Equation:

The waterway for channels shall be determined using Manning's Equation.

 $Q = 1.486 R^{2/3} S^{1/2} A$

Q = volumetric flow rate (cfs)

R = the hydraulic radius in feet

S = the slope of the energy grade line in feet per foot

n = roughness coefficient

A = cross-sectional area

The hydraulic radius, R, is defined as the cross sectional area of flow divided by the wetted flow surface or wetted perimeter.

Channel Cross Section and Grade:

The design capacity, the material in which the channel is to be constructed, and the requirements for maintenance determine the required channel cross-section and grade. The channel grade shall be such that the velocity in the channel is high enough to prevent siltation but low enough to prevent erosion. Velocities less than 1.5 feet per second should be avoided because siltation will take place and ultimately reduce the channel cross-section.

Side Slopes:

Earthen channel side slopes shall be no steeper than 3 to 1. Flatter slopes may be required to prevent erosion and for ease of maintenance. Where concrete lined channels are required, side slopes shall be no steeper than 12 to 1 with adequate provisions made for weep holes or subsurface drainage. Side slopes steeper than 12 to 1 may be used for lined channels provided that the side lining is designed and constructed as a retaining wall with provisions for live and dead load surcharge.

Channel Stability:

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- 1. All channels constructed shall have the following characteristics:
 - 1. It neither aggrades nor degrades beyond tolerable limits.
 - 2. The channel banks do not erode to the extent that the channel cross-section is changed appreciably.
 - 3. Excessive sediment bars do not develop.
 - 4. Excessive erosion does not occur around culverts, bridges or elsewhere.
 - 5. Gullies do not form or enlarge due to the entry of uncontrolled surface flow to the channel.
- 2. Channel stability shall be determined for an aged condition and the velocity shall be based on the design flow or the bank full flow, whichever is greater, using "n" values for various channel linings. In no case is it necessary to check channel stability for discharges greater than that from a 100-year return period storm.

SECTION 8 - DETENTION BASINS

Detention basins shall be designed in accordance with the following criteria:

Detention basins are typically designed to remain empty during dry weather and to backup or detain excessive runoff generated during a storm.

Fencing must be provided if deemed necessary by the Board. The Board must approve design and locations.

Basin Volume Design

- 1. A minimum basin volume shall be the difference in runoff volume discharged from the project area to the basin site between the 6-hour NRCS pre-development and post development 100-year storm. In cases where the volume requirement governs, the design calculations must not only show that the required volume has been created, but that the basin functions to detain the volume difference.
- 2. In many areas of the county the increased runoff volumes can be as critical, if not more critical, than the rate of discharge. CCDB will address this issue on a site-specific basis. All development submittals will be evaluated for the impacts of increased runoff and volume control. Satisfying the volume requirement may be met onsite, at approved off-site locations, or by purchase of volume in a Flood Compensation Bank if one is available in the watershed.
- 3. Maximum basin side slopes shall be 3:1, unless paved.
- 4. Low flow channels shall be grass if the channel grade is greater than 1.0%.
- 5. Basin design must include maintenance accessibility and responsibility.
- 6. The Professional Engineer shall address provisions for anti-seep collars, extended detention basins, wet ponds, soil bioengineering, baffles, outlet protection and length to width ratios.
- 7. Detention basins must be completely within a recorded permanent Detention Basin Easement.
- 8. Maps depicting the NRCS Hydrologic Soil Groups, Existing Land Use, and Projected Land Use for each watershed shall be evaluated to determine the appropriate surface condition factors for use in runoff calculations.

Basin discharge shall be designed with the following criteria:

1. Discharge control structures shall be multi-stage and capable of limiting 2, 10, and

- 100-year post-development discharges to the respective pre-development peak discharge rates or downstream system capacity and shall be constructed of concrete or approved alternate.
- 2. The emergency spillway shall be sized to accommodate a flow equal to the design overflow of the 100-year storm post-development discharge without overtopping the dam. Erosion protection must be provided for the spillway and receiving stream.
- 3. The dam elevation shall not be less than one foot above the 100-year storm storage and overflow elevation.
- 4. Appropriate downstream channel protection must be installed.
- 5. Storage, discharge, and routing calculations for the 2-, 10-, and 100-year discharges must be submitted for review.
- 6. Spillways shall be protected from erosion and shall employ energy dissipation, if necessary.
- 7. Detention basins shall be fully discharged within 36 hours after the storm event unless specifically approved by the Clark County Drainage Board.
- 8. The detention basin shall be the first item of construction prior to any other earth moving or land disturbing activities and must be designed to function as a sediment basin through the construction period. The Basin design must be checked for capacity due to additional runoff generated by disturbed site conditions.

Parking Lot Storage

Paved parking lots may be designed to provide temporary detention storage of storm water directly from the parking area, but are not appropriate for storing large volumes. Ponding should, in general, be confined to those positions of the parking lots farthest from the area served. Ponding areas must not conflict with handicapped parking and access routes. Such ponding areas should be exposed to sunlight in winter months to minimize icing. Storage depth must be limited so as not to conflict with parking lot use. Any detention facility utilizing a parking lot must take resurfacing and other parking lot maintenance activities into consideration during design.

Facility Maintenance Responsibility

Maintenance of drainage facilities during construction must be the responsibility of the land developer. Maintenance responsibilities must be documented by appropriate restrictive covenants to property deeds prior to final drainage plan approval. Routine maintenance is the developer's responsibility for a minimum of five (5) years after completion of the drainage facility. After that time, upon the approval of the County Engineer and the County Plan Commission, the County may accept responsibility for routine maintenance of the drainage facility. The permanent pool of a wet bottom basin is the responsibility of the developer or homeowners' association. Routine maintenance must, at a minimum, assure that the drainage facility performs the functions for which it was designed and constructed. Unless specifically accepted by the county, all drainage facilities must be privately owned and funded. The detention basin must be mowed a minimum of once a year and be kept free of trees and shrubs.

SECTION 9 – DOWNSTRAM RESTRICITONS

In the event the downstream receiving channel or storm sewer system is inadequate to accommodate the post-developed release rate provided above, then the allowable release rate shall be reduced to that rate permitted by the capacity of the receiving downstream channel or storm sewer system. Additional detention, as determined by the CCDB, shall be required to store that portion of the runoff exceeding the capacity of the receiving sewers or waterways.

If the proposed development makes up only a portion the undeveloped watershed upstream of the limiting restriction, the allowable release rate of the development shall be in direct proportion to the ratio of its drainage areas to the drainage areas of the entire watershed upstream of the restriction.

SECTION 10 - SINKHOLES

General

The use of sinkholes as storm water management is not permitted, unless there are no other alternatives.

Clark County does not encourage the use of natural sinkholes as outlets for drainage from developed areas and will avoid requests for modifications to sinkhole entrances. The proposed use of sinkholes as outlets for development must be approved by the CCDB and County Engineer.

For circumstances that have no other means for drainage, the following criteria shall be implemented:

Design

Specific design requirements for the use of sinkholes, when permitted, include but are not limited to:

- 1. The sinkhole shall have the volume to store a 100-year, 24-hour NRCS storm with a no outlet condition.
- 2. Storm water discharge into a sinkhole shall not be increased over its preexisting rate according to standards as established by the Clark County Drainage Board. Depressions containing sinkholes shall not be utilized for storm water detention unless no other alternatives exist.
- 3. Photographic evidence should be submitted to the Board showing the current condition of the sinkhole feature. If recent subsidence is evident, the sinkhole shall not be used for storm water drainage unless the feature has been evaluated by a Geotechnical Engineer, and he/she has determined that the feature can be treated so that significant future subsidence is not likely.
- 4. To confirm the suitability for an existing feature to accept a given runoff volume, the feature must be pump tested using at least 80% of the 100-year design storm for an 8-hour duration. The condition of the sinkhole before and after the pump test should be documented by a licensed professional engineer registered in the State of Indiana. Any evidence of significant subsidence that occurs during or after the test will be taken as unsuitability of the feature to accept runoff. To confirm that runoff into the sinkhole feature will not affect adversely adjacent properties, fluorescent dye should be injected into the sinkhole during the pump testing. A Geotechnical Engineer, registered in the State of Indiana, should be retained to make observations of the fate of the dye in the surrounding area.
- 5. Protective measures for the sinkhole inlet must be applied prior to the start of construction activities. Surface water runoff from stripped areas should be directed away from the sinkhole until the areas have been developed or ground cover has been installed and has become established.
- 6. An alternate means of surface water disposal must be provided in the event that the sinkhole ceases to accept runoff or significant subsidence occurs in the feature.
- 7. Storm water runoff from paved areas or structures shall not directly enter a sinkhole.

- Drainage plans shall be designed to route runoff through vegetative filters or other filtration measures before it enters a sinkhole. Such filters or filtration methods must be reviewed by the board.
- 8. A Geotechnical Engineer, licensed in the State of Indiana, must supervise the design and installation of sinkhole treatment measures. The engineer shall also observe installation of treatment measures and shall document that treatment measures comply with approved plans. The engineer shall be responsible for documenting significant subsidence or other changes in the existing sinkhole feature during treatment that may affect the effectiveness or practicality of the approved treatment method.
- 9. Any instances of significant subsidence must be fully documented and a Geotechnical Engineer, licensed in the State of Indiana, must supervise design of treatment measures, must inspect treatment installation, and must document construction of repairs prior to bond release.

SECTION 11 - FINAL DRAINAGE PLANS

Final drainage plans shall be submitted to the CCDB. Before final subdivision plat approval or before construction for all other developments, the final construction plans shall provide or be accompanied by calculations, maps and/or other descriptive material including:

Cover Sheet

- 1. Location map with the site outlined.
- 2. Title block: title of development, name and address of developer, name and address of Professional Engineer or Professional Land Surveyor, date of preparation, revision dates.
- 3. Index of sheets.
- 4. Engineer's or Land Surveyor's seals and signatures.
- 5. Construction notes.

Composite Drainage Plan

- 1. Topography: minimum scale 1'' = 100' with existing contours at two-foot intervals, NGVD datum. Contours to extend a minimum of 50 feet beyond property lines.
- 2. Proposed development: street rights-of-way, street names, street centerline stationing, lot lines, lot numbers, property boundary, existing drainage structures, proposed drainage structures (labeled by number or other designation) and easements with widths shown.
- 3. Hydrologic data: designate drainage areas (in acres) to individual inlets, and off-site drainage areas (acres), which generate through drainage.
- 4. Pipe chart: pipe number, drainage area, coefficient of runoff (c), time of concentration, intensity, discharge (Q), size, length, slope, capacity, velocity (refer to example #1).
- 5. 100-year FEMA and local regulatory floodplain and conveyance zone, if applicable, with flood elevations noted.
- 6. Identification of outlet system.

PLAN AND PROFILE (ROAD) SHEETS

Plan View

- 1. Catch basins: line and station number (structure number), grate type and elevation, invert elevation(s).
- 2. Pipes: length, size, type, slope, pipe number of designation.
- 3. Headwalls: type, invert elevation.
- 4. Ditches and swales: number or designation, type, stations.
- 5. Easements: type, size, existing with deed book and page numbers, proposed.

- 6. Utilities: existing and proposed (including sanitary sewers).
- 7. Other drainage structures to be labeled accordingly. (Refer to example #2 for matters pertaining to Items a. through g.).

Profile View

- 1. Storm lines and structures to be shown on road profiles.
- 2. Utility and sanitary sewer crossings.

Storm Drainage Profiles (pipes, ditches, box culverts)

- 1. Catch basins: station or number, type, grate type and elevation, invert elevation(s).
- 2. Pipes: length, size, type, class, grade, line number, headwater elevations for the 100-year storm (determined from inlet and outlet control analysis).
- 3. Ditches:

Type

Grade

Flow line elevation at grade changes (P.V.I)

Design depth

Manning's "n"

Slope

10-year velocities

100-year velocities

100-year discharge depths

Headwalls: type and invert elevation.

5. Existing and proposed ground surfaces. (Refer to example #3 for matters pertaining to Items a. through e.).

SECTION 12 – CHANGES TO THE APPOVED DRAIANGE PLAN

If the applicant or developer wishes to amend the site plan in any way after the drainage plan has been approved by the CCDB, the application must inform the CCDB (or an agent thereof) of the proposed change. If the CCDB or agent determines the change in the building or site plan significantly changes the drainage as proposed under the approved drainage plan, then the applicant or developer shall submit revised drainage plans for the CCDB's approval.

SECTION 13 – INSPECTION OF INFRASTRUCTURE

A registered engineer or land surveyor shall be employed by the developer and approved by the CCDB shall to conduct sufficient inspections to insure compliance with the specification set forth in this ordinance. Each phase of construction of the storm drainage improvements, as shown on the approved construction plans, shall be inspected. The CCDB or an agent thereof shall make a final inspection of said improvements before accepting said improvements for dedication to the County for permanent maintenance.

SECTION 14 - SUBMITTALS AND FEES

Plans shall be submitted twenty (20) working days prior to the scheduled Drainage Board meeting. In addition to the plans, the design professional shall submit the following:

15

- 1. Drainage Plan Review application
- 2. Drainage Plan Review Checklist
- 3. Detention Analysis Checklist

Items 1 through 3 can be found in Section 2 of the Appendix or can be picked up at the office of the County Surveyor.

ADOPTION OF ORDINANCE

This ordinance shall be in full force and effect ___ days after its final passage and adoption. All prior ordinances and parts of ordinances in conflict with this ordinance are hereby repealed.

PASSED AND ADOPTED this 2 day of July, 2010, by the following vote:

Commissioner

Commissioner

MIKE MOORE-ABSENT

Commissioner

Attest: Auditor of Clark County

APPENDIX

SECTION 1:

EXAMPLE #1 PIPE CHART

EXAMPLE #2
PLAN SHEET EXAMPLE

EXAMPLE #3
PROFILE SHEET EXAMPLE

EXAMPLE #1

	PIPE CHART									
PIPE NO.	A (ACRES)	Q (C.F.S.)			SLOPE (%)	V (FT/SEC)	Tc (MINUTES)	(IN/HR)	Q FULL (C.F.S)	V FULL (FT/SEC)
1										
2										
3								<u> </u>		
4							ļ			
5										
6									<u> </u>	
7									ļ	
8								<u> </u>		

EXAMPLE #2 33 10' DRAINAGE EASEMENT 4 140.48'~ 27" RCP C.B. STA. 13+16.04 LINE "1" = C/L REDBERRY JUNIPER COURT\ STA. 13+16.29, 14.25 LT INLET = 495.59 INV. = 491.01 ANG LINE -R50* R/W-"C" 28.52'~ 27" RCP 14+00 13+00 C.B. STA. 13+44.55 LINE "1" = C/L REDBERRY JUNIPER COURT COURT STA. 13+16.29, 14.25' RT INLET = 495.59 INV. = 491.30 27" RCP INV. = 491.55 24" RCP R/W-R34' 23.60'~ 2 C.B. STA. 13+68.16 LINE "1" = C/L REDBERRY JUNIPER COURT STA. 12+92.71, 13' RT INLET = 495.48 INV. = 492.44 36 10' DRAINAGE EASEMENT 115.80'~ 24" HANCOR, © 3.07% H.W. STA. 14+83.96 LINE "1" SLOPED AND FLARED INV. = 496.00**∭**15+00-16+00 -LINE "1" 15' DRAINAGE & WILLIAM EASEMENT

- DITCH FROM

13+00	8" SAN. RCP • 1.0% RCP • 3.77% - SEWER	REDE CHANGE 493.3	STA. 13+16.04 FI EL = 495.59 = 491.01 BERRY R COURT B. STA. 13+44.56 LET EL = 495.59 V. = 491.30 27° RCP V. = 491.55 24″ RCP B. STA. 13+68.16 LET EL = 496.48 V. = 492.44	
+00	NOTE: STATION 14+87.96 IS THE APPROXIMATE LOCATION WHERE THE CONCENTRATED FLOW COMES IN FROM MADOC ESTATES. On = 24.93 cfs One= 38.33 cfs	1) 115.80'~24" HANCOR	H.W. STA. 14+83.96 NV. = 496.0 STA. 14+87.96 LINE STA. 10+00 LINE	"1" == (-1"
00	Q ₀ = 1.48 of Q ₁₀₀ = 2.02 of Q ₁₀₀ = 2.02 of V ₁₀ = 2.89 ft/s V ₁₀₀ = 3.23 ft/s D ₁₀₀ = 0.41 ft D ₁₀₀ = 0.46 ft S ₁₀₀ = 0.48	V-DITCH SEED	A 15+35 497.54	
470	MATCH MATCH	490 H UNE	THIS SHEET	510

EXVWble #3

APPENDIX

SECTION 2:

DRAINAGE PLAN REVIEW APPLICATION

DRAINAGE PLAN REVIEW CHECKLIST

DETENTION ANALYSIS CHECKLIST

CLARK COUNTY, INDIANA DRAINAGE PLAN REVIEW APPLICATION

SECTION 1: PROJECT INFORMATION To be completed by the applicant.

Project Name:			Key Nun	nber:	
Project Address:			Deed Dr	awer:	Instrument
Subdivision Name/Lot	#:		Deed Bo	ok:	Page #:
			Plan for Comm		
Plan/plat previously sub	omitted?	(y/n)]	f yes, explain		
SECTION 2: CONTA	CT INFOR	MATION			
Check the appropriate box	to indicate who is	to be designated	as the responsible	entity for the las	nd disturbing activity.
□Property Owner: _			_	ontact Person	i:
Address:					
City:	State:	Zip:	Phone:()	Fax:()
Developer:			С	ontact Persor	n:
Address:					
City:	State:	Zip:	Phone:()	Fax:()
Design Firm:				Contact Person	n:
Address:					
Address:	State:	Zip:	Phone:()	Fax:(_)
T.	, being	the Design Pr	ofessional (Pro	fessional Eng	gineer and/or Professional
Land Surveyor of			(Name of	Development) s	shall submit Final Record
			nat) within thre	e months at	ter the completion of the
installation of the drain	age infrastruct	ure. Sia	nature		
		Sig	mature		
*Contractor:				Contact Person	n:
Address:					
City:	State:	Zip:	Phone:()	Fax:(_)
* If the Contractor is unk				onsibility of th	e responsible entity to
inform the Planning and	Zoning Office J	prior to final pla	t approval.		
Planning and Zoning	יב		I	Date Submitte	d:
Development Number					
Fee:			— Pa	aid:	
Seven copies of plans	and calculation	15:	(y/n)		
Drainage Board					
Date of Meeting:			Approved:	Deni	ed:
	0: -	C1 :		_ _	
	Signature of	Cnairman			

CLARK COUNTY, INDIANA DRAINAGE PLAN REVIEW CHECKLIST

Address		
Date	*Clark County Development	No
The purpose of this checklist is to expedite and fact needed for review. All items shall be checked as inc rejection of the submittal without review. REQUIRED ITEMS	luded or marked N/A. <u>The omission of</u>	required items may be cause j
CCDB Plan Review Application Location Map Registered Professional Stamp and Signature Property Boundaries Offsite Drainage Areas Drainage Flow Arrows Pipe, Length, Size, Slope, Type and Number Pipe Profiles for Through Drainage Adjacent Property Owners Existing and Proposed Easements Existing and Proposed Structures Erosion and Sediment Controls Headwater at Culvert Pipes (100-year) Standard Underground Utility Notes Existing and Proposed Topography and Adequate information/details pertaining	g to storage basin and drainage structur	Plan Date Revision Date Inlet Type Headwall Type Pipe Chart (refer to attached example) Drainage es vious Areas (clearly age Structures cation & Elevation
Design Professional's Signature	Date	

^{*} To be assigned by the Clark County Planning Commission

CLARK COUNTY, INDIANA DETENTION ANALYSIS CHECKLIST

Project Name	Project Name					
Submission Date	*Clark County I	Development No.				
	hecked as included or marked N/A.	This checklist gives the minimum requirements The omission of required items may be cause for				
Table of Contents						
Explanation of Analysis wi	th Assumptions					
Analysis of Downstream C	apacity Limitations					
Composite Drainage Area						
	Map(s) - Post-development					
Time of Concentration (To	c) Supporting Calculations - Pre-de	velopment				
	c) Supporting Calculation - Post-de					
	ve Number Calculations & Map - F					
Runoff Coefficient or Curv	ve Number Calculations & Map - I	Post-development				
	eak Flow Pre-development Runoff					
Calculations of 100-year Pe	eak Flow Post-development Runof	\mathbf{f}				
	00-year By-passing or Unmitigated	- Post-development				
Basin Volume Data (Eleva	tion/Storage)					
Basin Grading Plan						
Basin Outlet Structure Dat	ta and Construction Details					
	nt (Positive Through Drainage Ou					
	sis Check of Overflow Function (U					
	, Storage, Peak Elevation, Peak Inf					
	2, 10 and 100-year peak flows) Rou					
	lation is (Property Line Point Disc	harge)				
Complete Summary of Dra	unage Analysis					
the Drainage Ordinance of the C	City of Charlestown and that the pledge that to the best of my kno	nts meet or exceed the design standards of y were prepared under my supervision. I, owledge and belief, the products resulting				
Design Professional's S	Signature	Date				

Please use this checklist for all future submittals. Although we feel this checklist is complete, we recognize there is room for improvements, so please give us your feedback. By working together on this, we can make the review process better for everyone involved.

^{*} To be assigned by the County.

APPENDIX

SECTION 3:

SOIL GROUPS

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		Avontores promise of the central personal promise of the central personal p
D	AddB2	Avonburg silt loam, 2 to 4 percent slopes, eroded
30/12/14		Augustiniering gemanner of American Chores (A. 1922). The company of the company
D	AvB	Avonburg silt loam, 2 to 4 percent slopes
D	BbhA	Bartle silt loam, 0 to 2 percent slopes
B		TREATHERS OF STEED AND PROCESS TO SECURE OF SUCCESS AND ADDRESS OF STEED SECURIOR STEED SECURIOR SECUR
В	BcrAQ	Beanblossom silt loam, 1 to 3 percent slopes, rarely flooded
	2 BUW 2 1	Polynomical Edgam de la capacita del capacita de la capacita de la capacita del capacita de la capacita del capacita de la capacita de la capacita de la capacita del capacita de la capacita del capacita de la capacita de la capacita de la capacita del capacita del capacita del capacita del capacita de la capacita de la
С	BdB	Bedford silt loam, 2 to 6 percent slopes
	PHI WAY	Bedford silt loam, 2 to 6 percent slopes
C	BdoB	Bedford shi tomin, 2 to 6 percent support
C	BfcC3	Blocher, soft bedrock substratum-Weddel complex, 6 to 12 percent slopes, severely eroded
		A CHEADAN SOUTH ON A STATE OF THE WEST AND A STATE OF THE
C	BnyD3	Bonnell clay loam, 12 to 22 percent slopes, severely eroded
		Compalition of the Court of the Court of Court o
C	Во	Bonnie silt loam
eo/	ne markatan	E IRANDIO SITUTO MALLA CONTROLLA CON
В	BvoG	Brownstown-Gilwood silt loams, 25 to 75 percent slopes
e.		Calleveline Rostooline (op copidle : Mic/sobjectents in hes.
C	CcB2	Cincinnati silt loam, 2 to 6 percent slopes, eroded
	7 (CC2)	Cincinnan sitticam carole procedus anescerous
C	CcC3	Cincinnati silt loam, 6 to 12 percent slopes, severely eroded
0	CiDel	Cincinnati silt loam, 12 to 18 percent slopes, severely eroded
C	CcD3	Cincinnati sili loam, 12 to 18 percent slopes, 30000)
	CldC2	Cincinnati-Blocher silt loams, 6 to 12 percent slopes, eroded
С		

C	CldC3	Cincinnati-Blocher silt loams, 6 to 12 percent slopes, severely eroded
		Cleuron still barr 200 3
C(drained)	ClfA	Cobbsfork silt loam, 0 to 1 percent slopes
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C	ComC	Coolville silt loam, 6 to 12 percent slopes
	(Vojni)	A Com Ville Raed in Complex 1921 of the partial value is a series of the
	ConC3	Coolville-Rarden complex, 6 to 12 percent slopes, severely eroded
D	CoG	reproduktions all loam 12 m. 15 section is long.
His section of		Corydon stony silt loam, 25 to 70 percent slopes
В	CP3	Chair all abstactores and abstacle and a second a second and a second
B The state of the	CspB2	Crider silt loam, 2 to 6 percent slopes, eroded
C	CrB2	Content of the Approximation of the Content of the
	CIB2	Crider silt loam, 2 to 6 percent slopes, eroded
C	CrC2	
	CICZ Covoroves	Crider silt loam, 6 to 12 percent slopes, eroded
C	CrD2	Ggreer silkiloam core (2 percentisionis, se vorebarrogata 3 a.a.)
2004-2004	Cide Coldenies	Crider silt loam, 12 to 18 percent slopes, eroded
В	CtrB2	Crider silt loam, karst, undulating, eroded
	Television 1	Critici siii loali, karsi, undulating, eroded
В	CxgC3	
	orges Towns	Crider-Haggatt complex, 6 to 12 percent slopes, severely eroded
В	CxhC2	Crider-Haggatt silt loams, 6 to 12 percent slopes, eroded
	CXAC2 S	Giller-Habeall's II floating was statelling to open as a second
В	CwaAQ	Cuba silt loam, 0 to 2 percent slopes, rarely flooded
:C24345W		Dearith Clay Cam 2016 Septem 1606
B	DdsAW	Dearborn silt loam, 0 to 2 percent slopes, occasionally flooded, very brief duration
	Divez	Deputy frappis sill forms of the process of the fraction from the first of the firs

SG	Symbol	Soil Name
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	EbpD2	Eden silty clay loam, 12 to 25 percent slopes, eroded
		TENEDISTICATION OF TOTAL CONTROL OF THE CONTROL OF
	EesA	Elkinsville-Millstone silt loams, 0 to 2 percent slopes
	PANESHIND AND	
		Elkinsville-Millstone silt loams, 18 to 40 percent slopes, rarely flooded
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		A SIGNATURE ACTORISE SID TO DOTO A CONTRACTOR OF THE SIGNATURE OF THE SIGN
3	EesC2	Elkinsville-Millstone silt loams, 6 to 12 percent slopes, eroded
		nature of the state of the stat
))	FcG	Fairmount stony silty clay loam, 25 to 70 percents slopes
	r izanezara	Gillippe in Lionning Charles are researched to the second
C L	GIC3	Gilpin silt loam, 6 to 12 percent slopes, severely eroded
		Gilpin silt loam, 12 to 18 percent slopes, severely eroded
C	GID3	
	GIE	agriforn ei Libarti (1846) : percentelloges (Philes)
В	GgbG	Gilwood-Brownstown silt loams, 25 to 75 percent slopes
B	38 (60 Z)	p. Gilvicon Wigner and no and the proper constitutes reforced to the constitution of t
В	GgfD	Gilwood-Wrays silt loams, 6 to 18 percent slopes
er eveny	Seriomics	Somewhite with a submit a common progression and the submit and th
	GrA	Grayford silt loam, 0 to 2 percent slopes
В	UIA	
В	GrC2	Grayford silt loam, 6 to 12 percent slopes, eroded
		Company of the invitation of Company and the property of the latest and the company of the compa
B	GrD2	Grayford silt loam, 12 to 18 percent slopes, eroded
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В	GrE2	Grayford silt loam, 18 to 25 percent slopes, eroded
answer!		
	GyaD2	
В	GyaD2	Gray to a constraint of the co

HIS OFF	s Symbol/	
В	GyaD5	Grayford silt loam, 12 to 25 percent slopes, gullied
Eller de la company		Gravford silt loam, karst, hilly, eroded
В	GykD2	Graytord silt loam, karst, lilly, eroued
C	HaC2	Hagerstown silt loam, 6 to 12 percent slopes, eroded
		tanacers transmit to the real stems to the second that the sec
С	HaE2	Hagerstown silt loam, 18 to 25 percent slopes, eroded
	Professional Control	Papuagers from the life of later light in the later of th
С	HcD3	Hagerstown silty clay loam, 12 to 18 percent slopes, severely eroded
	MOTERAL DE	e directorio vin si Liva la ricamente del Sonerio e del Britante del Propositio del Charles del Companyo del Co Companyo del Companyo del Compa
C(B/C)	HtzD3	Haggatt-Caneyville complex, 12 to 25 percent slopes, severely eroded
COLO	HtwD2	Haggatt-Caneyville silt loams, 12 to 25 percent slopes, eroded
C(B/C)	ntwD2	Traggat-Carloyvino sit touris, 12 to 20 per entrope, touris and the same sit carrow in the
C	HcaA	Hatfield silt loam, 0 to 2 percent slopes
	a-illi disz	and the same of the factor of the factor and the state of the factor of
С	HceC3	Haubstadt-Shircliff complex, 6 to 15 percent slopes, severely eroded
		A PHAID THAIR SIDICHT STUID AND TO SUICE PERCENCIO ESPERO DE UNITARIO DE LA CARRA DE LA CARRA DE LA CARRA DE L La Carra De La
В	Hd	Haymond silt loam
	A THE PARTY	Haymond silt loam, 0 to 2 percent slopes, frequently flooded, very brief duration
В	HcgAV	Haymond silt loam, 0 to 2 percent slopes, frequently flooded, very brief duration
C	HeA	Henshaw silt loam, 0 to 2 percent slopes
ica vet	SOCIETA	AN HICKSTV-III Toam (10 to 25 spercent slopes of the state of the stat
C	HerE	Hickory-Bonnell complex, 12 to 25 percent slopes
C T	e HōAV	Trosmersin to am julo 2 percent superation in the control of the c
C	HoB2	Hosmer silt loam, 2 to 6 percent slopes, eroded
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SG	Symbol	Soil Name
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	HoD2	Hosmer silt loam, 12 to 18 percent slopes, eroded
		Humington's Milonon.
	HufAK	Huntington silt loam, 0 to 2 percent slopes, occasionally flooded, brief duration
	√s IndBΩv = Σ	Dentings silvingan 2007 operands libras let orled).
	JafC2	Jennings-Blocher hard bedrock substratum, silt loams, 6 to 12 percent slopes, eroded
	A THE STATE	Andromic Schlosife: In all he do also in sur him all viloums care if a person surprise several le collèction d
	JeA	Jennings silt loam, 0 to 2 percent slopes
2400 MX	Man De Sa	a Marining Sault Good Output percent slopes products
C	JhB2	Jennings silt loam, heavy subsoil variant, 2 to 6 percent slopes, eroded
		THE DINE SURFACE CONTROL OF THE PROPERTY OF TH
C	JhC3	Jennings silt loam, heavy subsoil variant, 6 to 12 percent slopes, severely eroded
		Westings of the four the first of the first
D	JoA	Johnsburg silt loam, 0 to 2 percent slopes
		TELEMOTIENCE Plage at Company il Becomples Usafor 25 major differential postare presidential and the comples usafor 25 major differential and the complex usafor 25 major differential and
		Knobcreek-Haggatt-Caneyville complex, 6 to 12 percent slopes, severely eroded
C(C/B/C)		Anjorofiek Havigent Cane volles il etams 10 notempere en elapes e caled a
	KxpD2	Knobcreek-Haggatt-Caneyville silt loams, karst, hilly, eroded
C Varcidae i	KAPDE	NO AND THE PROPERTY OF THE PRO
) KxoC2	Knobcreek-Navilleton-Haggatt silt loams, karst, rolling, eroded
C(C/B/B) NXUCZ	2. ADmissiers (Tuesan Wisk species). Stopes to repain (1) A 10 species of E-point (1) (1) (1) (1) (1) (1)
		26 graded rarely flooded
C	MdqDQ	
	Min	and a second of the second of
С	McgC2	
	NAME OF THE PARTY	12 - see t clopes severely eroded
C	McpC3	Markland sitty clay to air, o to 12 percent stepes,
Q V	Mho?	
C	MhyA	Medora sur Ioani, o to 2 percent stopes

HSGL	(1500mino)	
С	MhyB2	Medora silt loam, 2 to 6 percent slopes, eroded
	Chvin/Carry	Mario asiluloam (616 lisperaents) pesperioticular.
C	MhyC3	Medora silt loam, 6 to 12 percent slopes, severely eroded
	//or help	w With Condition 1680 Days (1985) 1882 And 1882
D	MsvA	Montgomery silty clay loam, 0 to 1 percent slopes
		Company of the Construction of the Constructio
С	NaaB2	Nabb silt loam, 2 to 6 percent slopes, eroded
		Newark silt loam, 0 to 2 percent slopes, occasionally flooded, brief duration
C	NbhAK	Newark shit toam, o to 2 percent stopes, decade and sails and sail
	Ofbaw PcrB2	Pekin silt loam, 2 to 6 percent slopes, eroded
C	PUIDZ	Pekint site totali, 2 to 0 porter supply evolution and the state of th
C	PcrC3	Pekin silt loam, 6 to 12 percent slopes, severely eroded
С	PhaA	Peoga silt loam, 0 to 1 percent slopes
	e juliot sa	Sells quarry 1960 and the sell of the sell
	Ppu	Pits, sand and gravel
		at Thin Education (1995) and the state of the
C	RblD3	Rarden silty clay loam, 12 to 18 percent slopes, severely eroded
	(P. CRB mDb	PERMIENSICALIA VOICER ROBERTEIL STORE SEU IL CARROLLE CONTROLLE CO
C	RdC2	Rarden silt loam, 6 to 12 percent slopes, eroded
26 451	Z RADŽ	c Randen situloami-12/10-18-pernent slopes rerotted y application of the state of t
C	ReC3	Rarden silty clay loam, 6 to 12 percent slopes, severely eroded
C	va Redia	XENT arden silryclay loam; 102001101per ehitilores, severely erdded a
D	RkF	Rockcastle silt loam, 18 to 55 percent slopes
70(D/B)	AP AROLG	Rossmoyne silt loam, 0 to 2 percent slopes
C	RoA	Rossmoyne silt loam, 0 to 2 percent stopes

HSG	Symbol	Soil Name
	Robs	ANTOS MOVIDES I I SUBMITATO CONTROLLINO DE SEVERE I ACTO CONTROLLINO DE SE
B	RtcA	Ryker silt loam, 0 to 2 percent slopes
#602WE35W	ESPERIOR S	Riversijeloanikalok percentelijbet eradent at die kan die de
	D - D2	Ryker silt loam, karst, undulating, eroded
В	RzrB2	Proversitional, and discontinuous percent stops would
	Ro (Ca	
В	RztC3	Ryker-Grayford silt loams, 6 to 12 percent slopes, severely eroded
		STOROGENERAL DESIGNATION OF THE STATE OF THE
B	RzvC3	Ryker-Grayford silt loams, karst, rolling, severely eroded
		TSGGTISTOTIC SUICLOSTIC ZALDIANDERGIN TSTEDESSELDTED
	SfyB	Shircliff silt loam, 2 to 6 percent slopes
C	olyb Western	To any alternation of the control of
С	SoaB	Spickert silt loam, 2 to 6 percent slopes
CVI	Stall	Spicker filolism, thirade slub Aneroshis Uges has
C(C/B)	SolC2	Spickert-Wrays silt loams, 6 to 12 percent slopes, eroded
10 PM		Survivered (Albami, Orto Alberta entista per a resultant de la companya de la companya de la companya de la comp
C	StdAW	Stendal silt loam, 0 to 2 percent slopes, occasionally flooded, very brief duration
C		STEEDUSTE KANDE OND SEPERATURA PROMINENT CONTRACTOR OF THE SECOND CONTR
(Cartina	14.5(0.00)	
C	ThbD5	Trappist silty clay loam, 6 to 18 percent slopes, gullied
		Transfit Deput verment executed penents in the result of the control of the contr
D(C/D)	ThcD3	Trappist-Rohan complex, 12 to 25 percent slopes, severely eroded
TO CONTRACT OF THE PARTY OF THE		
C	TrC2	Trappist silt loam, 6 to 12 percent slopes, eroded
nereensel		
С	TrD2	Trappist silt loam, 12 to 18 percent slopes, eroded
E STATE	TO THE REAL PROPERTY.	and a special state of the stat
110000000000000000000000000000000000000	UaoAK	Udifluvents, cut and filled-Urban land complex, 0 to 2 percent slopes, occasionally flooded, brief duration
	a dara	
В	UnB2	Uniontown silt loam, 2 to 6 percent slopes

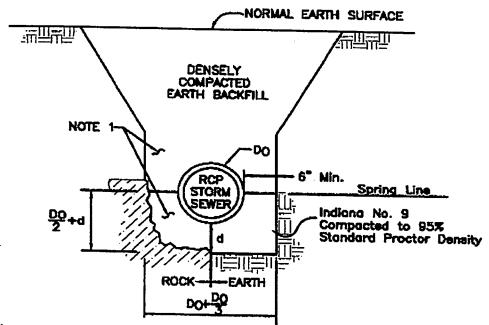
HSGA	Symbol 2	
В	UnC2	Uniontown silt loam, 6 to 12 percent slopes
	Alleda V	(Nehan land wovens elaveys) benanin permolex l'acceptatione entre centre le presente le presente le presente l L'acceptation de la company
	UnsB	Urban land-Udarents, clayey substratum, complex, hills, 2 to 10 percent slopes
	AUG/P	Authan Induntarents dag gant substratum, complex altiplant dagt delectivitares.
	UnpA	Urban land-Udarents, loamy substratum, complex, terrace, 0 to 3 percent slopes
		puritain janduvilli enis killy enistratum adampus yuenase Ogokopendenia lupose uti jisi y
	UndAY	Urban land-Udifluvents complex, leveed, 0 to 2 percent slopes
	Na Vi	Cawairelaine siluibian in a chair the second of the second
C	WaaAV	Wakeland silt loam, 0 to 2 percent slopes, frequently flooded, very brief duration
(C)		Walkermit silkitam Otes percentsieries occasionalizatie odelt vendbrendbrendt.
A CONTRACTOR OF THE PARTY OF TH	W	Water
	V	wedterfisit inam emploine einges einden en e
C/D	WcG	Weikert channery silt loam, 35 to 90 percent slopes
C		Wennach Sill Cabao 1672 Fercent slopes
В	WhcD	Wellrock-Gnawbone silt loams, 6 to 20 percent slopes
	-WiB2	AMNEIJITE/TITESTITEVILAMEZAOIG/BUTTETT SIDTES ET STEEL
В	WhC2	Wheeling fine sandy loam, 6 to 12 percent slopes, eroded
	Z TVIAV	zenvheelinesrikteane (Orderpeteern sterpes
В	WIB2	Wheeling silt loam, 2 to 6 percent slopes, eroded
	iwiG2	Wheeline stinleamidate percentstopenetodenex
B	WID2	Wheeling silt loam, 12 to 18 percent slopes, eroded
C 4	#White	Wincombstitican Oto sperdent slopes 1975
В	Wm	Wilbur silt loam
	VASiowa = 3	William Guiov perentalones requently poded very of let duration.
В	WokAW	
	ŢŢŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖŖ	TWinkinam ono 2 speteint slippes (loedational vallotides, de vibrier authrition)
C	ZaB3	Zanesville silt loam, 2 to 6 percent slopes, severely eroded
	#Zi62	au Azancsvilles ikiloam sotto ile theroenis lõpes seroided se ale a saat a saat a saat a saat a saat a saat a A saat a saa

HSG Symbol Soil Name
TO A CONTROL OF THE PROPERTY O
C ZaD2 Zanesville silt loam, 12 to 18 percent slopes, eroded
TANCE AND A ZADIS AND ZADIS UNICEDINIDATINE TOTAL PROPERTIES TO SERVICE STATES AND A SERVICE
D Zp Zipp silty clay

APPENDIX SECTION 4:

PIPE BEDDING DETAILS

d = 4" for 24" dia. thru 48" dia. d = 6" for 54" dia. thru 72" dia. D_O = Cutside Pipe Diameter



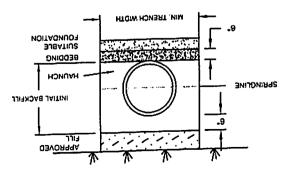
STORM SEWER TRENCH & BEDDING DETAIL

CATIONS

MINIMUM COVER FOR NON-TRAFFIC A.

MINIMUM COVER FOR TRAFFIC APPLICATIONS

SIN STANDARD TRENCH DETAIL



PER AASHTO SECTION 30 VECHICLE LOADING CONDITIONS **WINIMUM RECOMMENDED COVER BASED ON**

-87	54.	54.	.09
.87	54.	"ZI	15 48.
(NOT 81)	CONSTRUCTION (NOT 2S)	H-25 or HS-25	PIPE OIA.
	NE FOYDING CO	SURFACE L	

PER ASTM D2321 & AASHTO SECTION 30 RECOMMENDED MINIMUM TRENCH WIDTHS

110. (38.)	96. (80.)	.09
100. (810.)	90. (e9.)	-87
(.08) .96	15. (e0.)	45.
85. (6,-10.)	(2.7.5)	.96
(2.09)	20. (49.)	.0€
(2.7.s)	48" (4'-0")	54.
(48.)	37" (3'-1")	18.
(40)	34. (510.)	.gı
44. (38.)	35. (58.)	15.
45. (36.)	30. (56.)	-01
POOR SOIL	COOD SOIL	(.a.i)
MIN. TRENCH WIDTH		NIDE OIV
	101010170	1771 IAI I C

AMOOMM

BTAOVBR

СНКЮ

СИКД

COVER MOUND BACKFILL TO MINIMUM COVER FOR CONSTRUCTION TRAFFIC

MIM' TRENCH WIDTH

SERINGLINE

PT MINUS PAYEMENT DEPTH

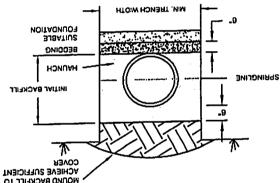
HOITAGNUDA

INITIAL BACKFILL

PAVEMENT BASE

SUITABLE

SEDDING



PER AASHTO LRFD DESIGN SPECIFICATIONS SECTION 12 RECOMMENDED MINIMUM / MAXIMUM BURIAL DEPTHS

HT930 JAIRUB XAMWIM	PIPE DIA.
(.TR)	(.0.1)
1.0' / 20'	.9-1
1.0.1	*01-8
1.0.1 19"	15-18.
1'0.\ 12.	S4-30.
1.0.1	.Zr-9E
1.0.1	*09-81

SPANNO NUMARO

REV

#5NIWARG

NOTTHINDSBO

DESCRIPTION

BEDDING HONDAH SPRINGLINE BACKFILL JAITINI .9 BACKFILL **GBVOR99A** RIGID PAVEMENT, H FLEXIBLE PAVEMENT, H MIN' COVER TO MIN. COVER TO PAVEMENT BASE

AND PRATICIPATE WITH INSTALLATION QUALITY ASSURANCE ON AN AS-NEEDED BASIS. ANSHTO MASS, LATEST EDITIONS PIPE MANUFACTURERS SHALL BE PRE-APPROVED BY MSD HIGH-DENSITY POLYETHYLENE (HDPE) MANUFACTURED ACCORDING TO ASTM F2306 OR 1. CORRUGATED PLASTIC PIPE FOR STORM WATER CONVEYANCE SHALL BE DUAL WALL

POUNDATION

BJBATIUS

(SEE TABLE)

MIN TRENCH WIDTH

REPRESENTATIVE FOR ADDITIONAL INSTALLATION GUIDANCE. GRAVITY FLOW APPLICATIONS, LATEST EDITION, CONTACT LOCAL MANUFACTURING WHO THE REPUBLICATION OF THERMOPLASTIC PIPE FOR SEWERS AND OTHER INSTALLATION GUIDANCE CAN BE OBTAINED FROM ASTM DS321, STANDARD PRACTICE FOR 2. ALL HOPE PIPE SHALL BE INSTALLED PER MSD STANDARDS, SUPPLEMENTAL

MATERIAL AS SPECIFIED BY THE ENGINEER AND/OR THE OWNERS REPRESENTATIVE. EXCAVATE TO A DEPTH REQUIRED BY THE ENGINEER AND REPLACE WITH SUITBREE 3 FOUNDATION WHERE THE TRENCH BOTTOM IS UNSTABLE, THE CONTRACTOR SHALL

DEPTH HOTED. 4 BEDDING: STANDARD BEDDING MATERIAL SHALL BE A CLASS I (A) or A3), CRUSHED

9. BEODING AND BACKFILL MATERIAL SHALL BE FREE OF DEBRIS, BOULDERS, AND FROZEN PIPE UNLESS APPROVED BY ENGINEERING. CRUSHED AGGREGATE, BACKFILL SHALL EXTEND NOT LESS THAN B-INCHES ABOVE THE 5 INITIAL BACKFILL. STANDARD BECDING MATERIAL SHALL BE A CLASS (A) of A3).

A BACKFILL MATERIAL IS TO BE PLACED IN 6-INCH LIFTS AND CHECKED INTO THE HAUNCH LUMPS, MAXIMUM DIAMETER OF BACKFILL AGGREGATE IS 1.5-INCHES.

AREA TO ENSURE MAXIMUM CONTACT WITH THE PIPE.

FACILITATE DRAINAGE. WHERE DIRECTED BY THE ENGINEER, THE PERIMETER OF THE TRACKL BY THE PENCINE FABRIC MSO STANDARDS, BEDOING AND BACKFILL MATERIAL SHALL BE OPEN GRADED TO B. IN THE CASE HIGH GROUNDWATER, THE TRENCH SHALL BE DEWATERED ACCORDING TO

SANDS (SEE CHART) INCREASED WHERE IN-SITU SOILS ARE UNSUITABLE; SUCH AS SOFT CLAYS OR LOOSE 9 WHERE DIRECTED BY THE ENGINEER, THE MINIMUM TRENCH WIDTHS SHALL BE

ENSURING ADEQUATE COVER. (SEE CHART) 10. DURING CONSTRUCTION, PREVENT DAMAGE TO THE PIPE OR ENCASEMENT BY

REPRESENTATIVE IS ENCOURAGED TO MAKE PERIODIC VISITS DURING INSTALLATION. MANUFACTURER'S REPRESENTATIVE PRIOR TO INSTALLATION, MANUFACTURER'S THE CONTRACTOR IS REQUIRED TO CONDUCT A PRE-CONSTRUCTION MEETING WITH

- 1	100		#3(4())(40)
	مجمع ا 10 ا	DW. ENSTEYS SDAMAND SOMANDA	NOTTALLATION
	SIN		MOTTATIATOM
	STI CHARD	Transport of the second of the	FOR HDPE STORM PIPE
	ENG	HILLIARD, OHIO 43026	BUILD A CORD OF THE WAY IN IN
	U113 we e-	THE THE STATE OF T	STANDARD DRAWING DETAILS
	05/21/2008		
			10811

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PROJECT APPLICABLE NATIONAL, STATE, OR LOCAL REQUIREMENTS AND TO ENSURE THAT THE DETAILS PROVIDED HEREIN ARE ACCEPTABLE FOR THIS CONSTRUCTION. IT IS THE DESIGN ENGINEERS RESPONSIBILITY TO ENSURE THE DETAILS PROVIDED HEREIN MEETS OR EXCEEDS THE RECOMMENDATIONS AND ARE NOT SPECIFIC FOR THIS PROJECT. THE DESIGN ENGINEER SHALL REVIEW THESE DETAILS PRIOR TO PROJECT, NOR HAS ADS INDEPENDENTLY VERIFIED THE INFORMATION SUPPLIED. THE INSTALLATION DETAILS PROVIDED HEREIN ARE GENERAL INTENDED TO DEPICT THE COMPONENTS AS REQUESTED. ADS HAS NOT PERFORMED ANY ENGINEERING OR DESIGN SERVICES FOR THIS SI DIMANDE SIMT. ROA OT GEGVORY NOTAMACHI IN DETAIL BASED ON INFORMATION PROVIDED TO ADS. INITID DRAWING IS O 2007 ADS, INC.